

Advance on Unloading Rock Mass Mechanics

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CONTENTS

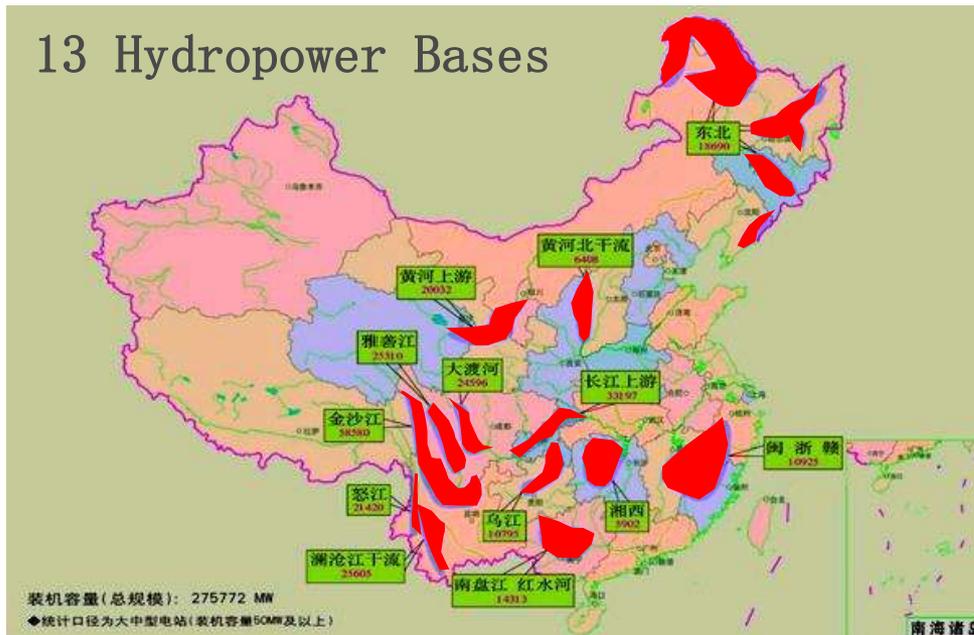
- 1、 Research Background
- 2、 Methodology
- 3、 Research Contents
- 4、 Engineering Application
- 5、 Research Platform

1. RESEARCH BACKGROUND

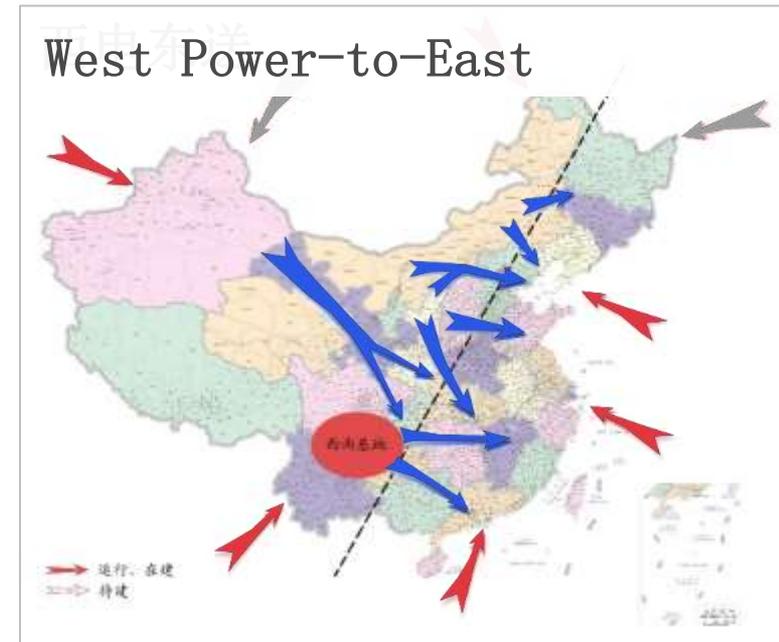
1.1 Industry Background

Over the past few decades, China has successfully built a number of hydropower stations. According to the National Energy Development Projects (2006-2015), plenty of hydropower based constructions have been built in China.

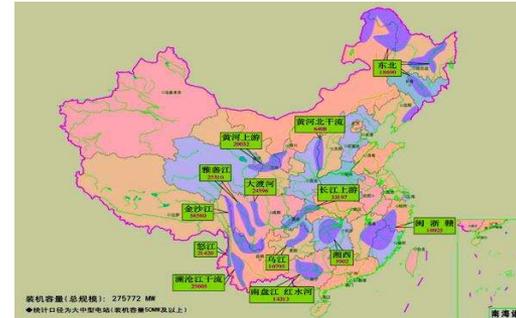
13 Hydropower Bases



West Power-to-East



1. RESEARCH BACKGROUND



Hydropower Bases



1. RESEARCH BACKGROUND

1.2 Engineering Background

- Three kinds of rock masses

Slope



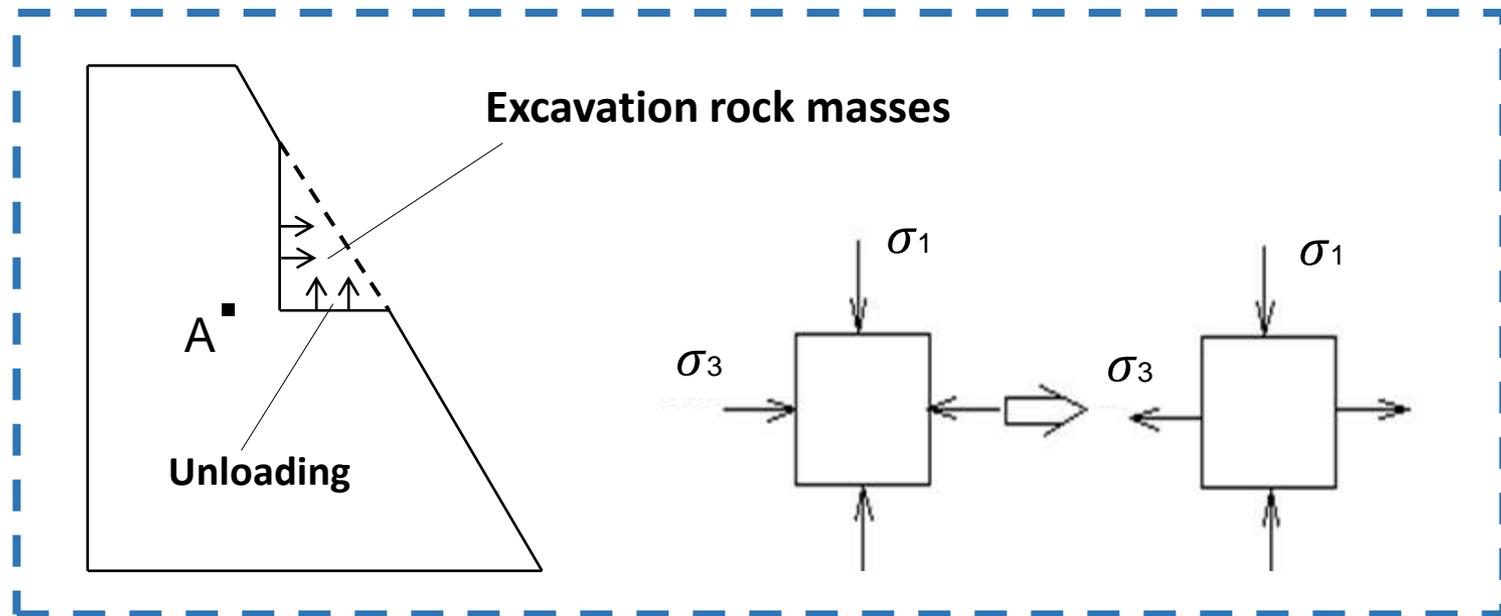
Foundation



Tunnel

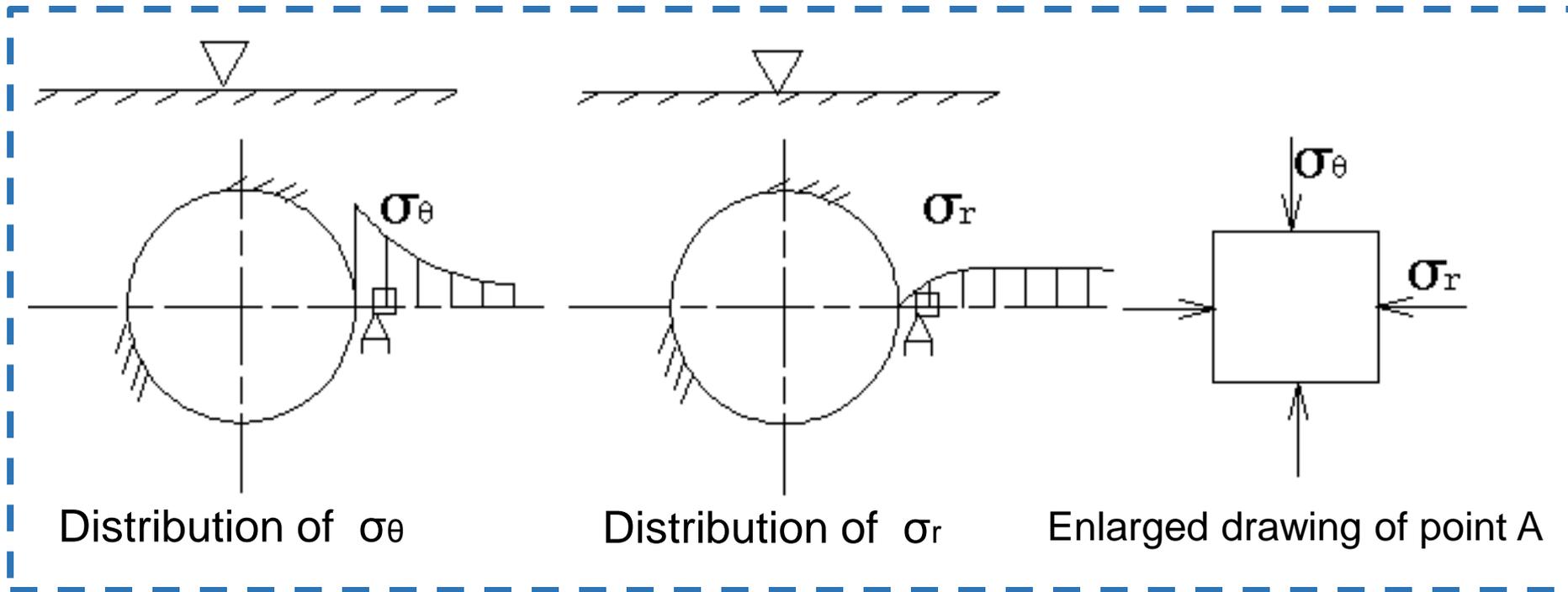


Example 1: Slope Engineering



- For point A
- Before excavating: $\sigma_1, \sigma_3 \rightarrow$ loading condition.
- After excavating: $\sigma_1 \rightarrow$ loading condition, $\sigma_3 \rightarrow$ unloading condition.

Example 2: Tunnel Engineering

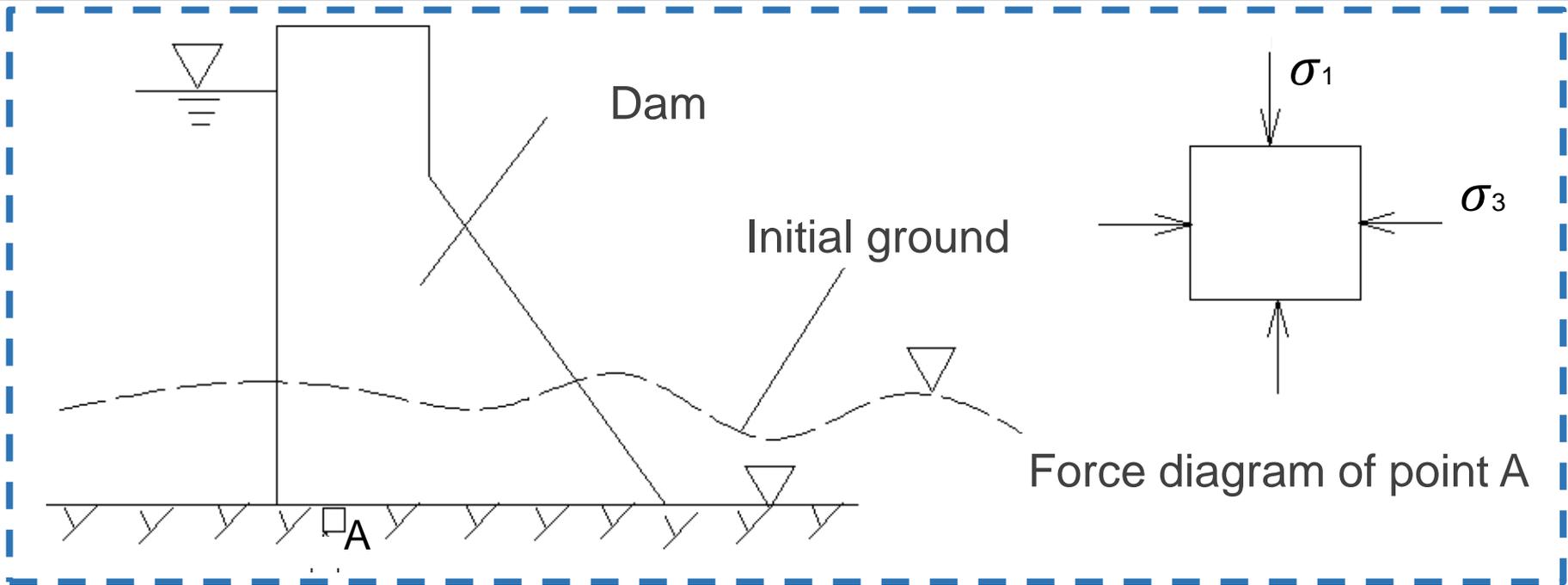


- For point A

Before excavating: $\sigma_\theta, \sigma_r \rightarrow$ loading condition.

- After excavating: $\sigma_\theta \rightarrow$ loading, $\sigma_r \rightarrow$ unloading.

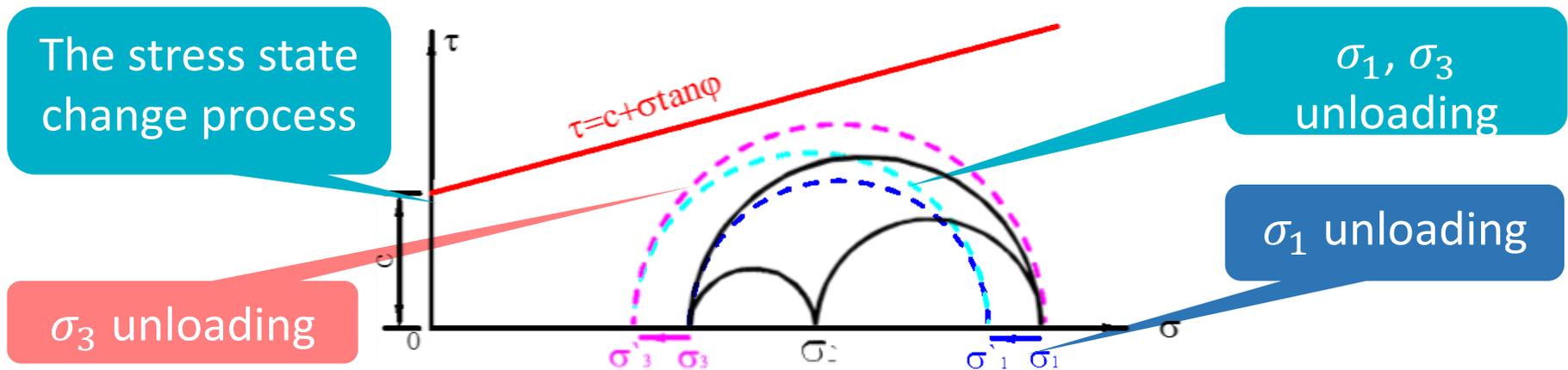
Example 3: Foundation Engineering



- For point A
- Before excavating: $\sigma_1, \sigma_3 \rightarrow$ loading condition.
- After excavating: $\sigma_3 \rightarrow$ loading, $\sigma_1 \rightarrow$ unloading condition.
- Dam construction: $\sigma_1, \sigma_3 \rightarrow$ loading condition

1. RESEARCH BACKGROUND

Different unloading paths of the unloading rock masses



- In different forms of rock masses engineering, the mechanics action process of the rock masses is different.
- The mechanical properties of rock masses are varied during the process of bearing alternative forces.
- There are essential distinctions between the mechanical characteristics of rock masses under unloading and loading conditions.

1. RESEARCH BACKGROUND

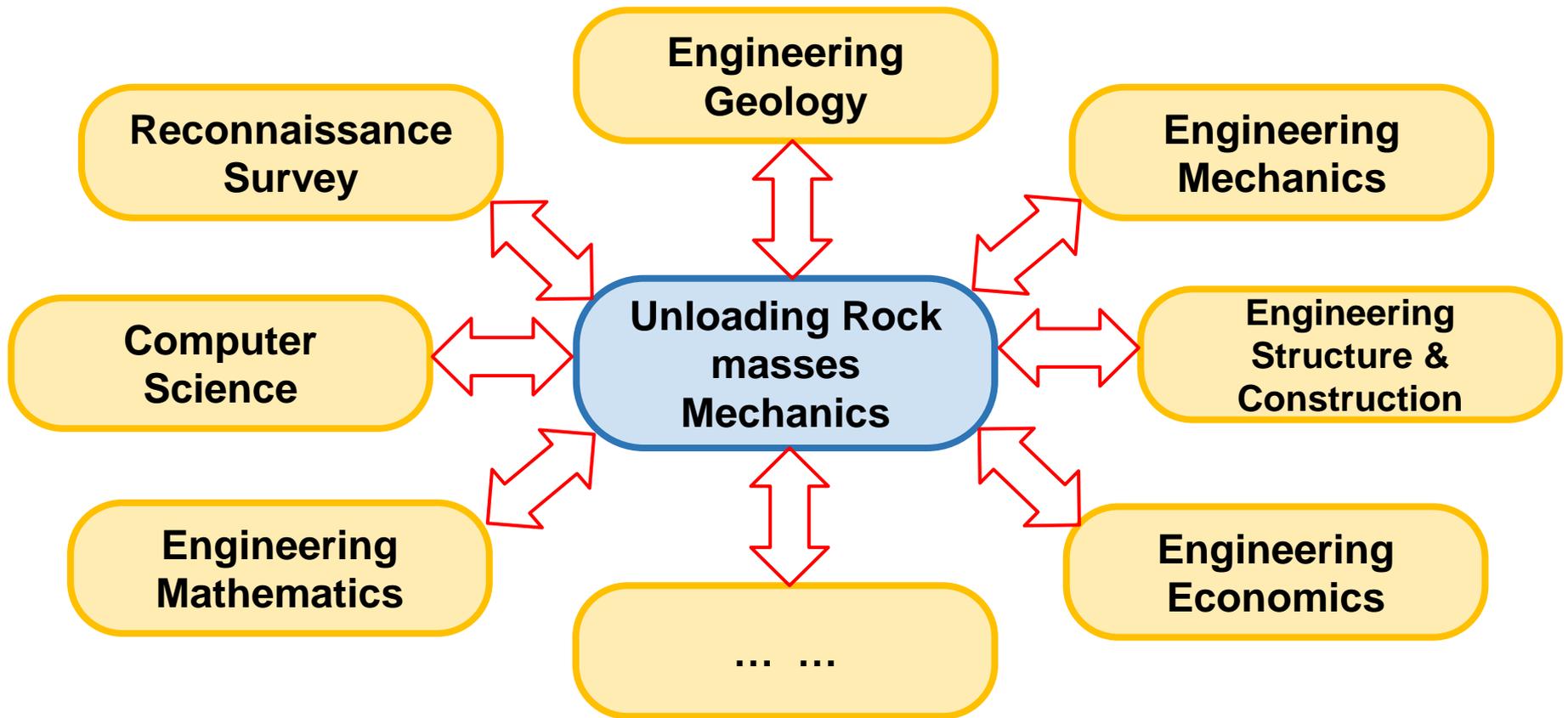
The discrepancy between the deformations computed by using traditional method (without considering unloading condition) and the actual deformations are shown in this table.

Engineering	Actual deformation	Calculating deformation by traditional method
Lianzi cliff dangerous rock body in the Three Gorges	2.17m	10cm
Jinchuan mine slope	1.52m	20cm
Ertan hydropower station	17.57cm	3cm
The Three Gorges permanent lock slope	17.38cm	3.47cm

Considering the above all, one should study the unloading mechanics to solve those problems as a new approach.

2 Methodology

Multi-crossed Disciplines



2 Methodology

Research Procedure

Understanding of Rock Masses



Utilization of Rock Masses



Protection of Rock Masses



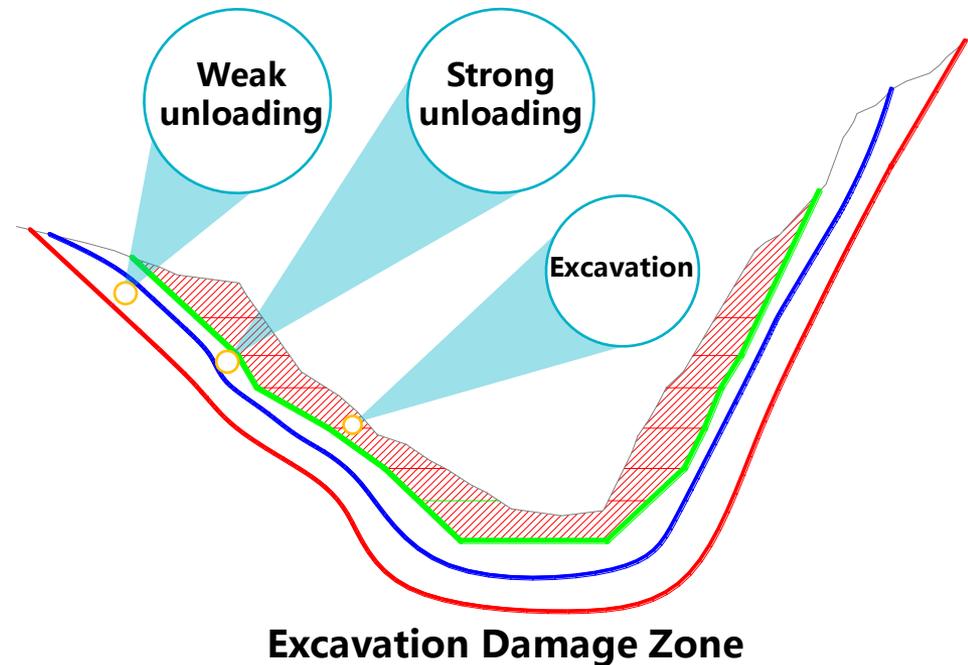
Monitoring of Rock Masses

3 Research Contents

(1) Division of Excavation Damage Zone

The essential of unloading rock masses is that the adjustment of the internal stress state of the rock masses leads to the damage of rock masses quality during the excavation process.

Moreover, the stress adjustment in different rock masses region changes at different levels, corresponding to the different deterioration degree of rock masses quality. Therefore, how to divide the excavation damage zone becomes one of the key problems in the study of unloading rock masses.

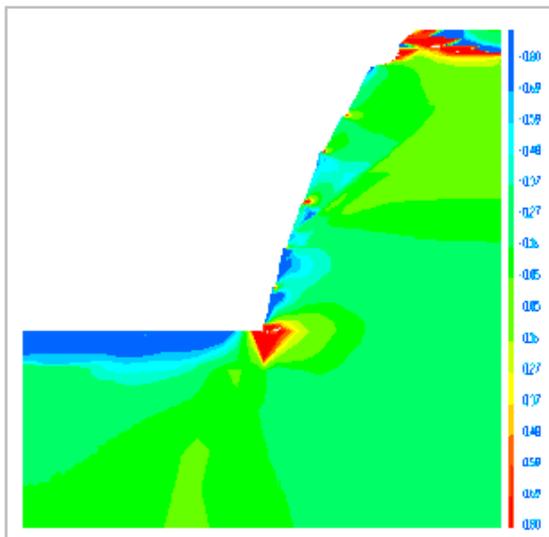


3 Research Contents

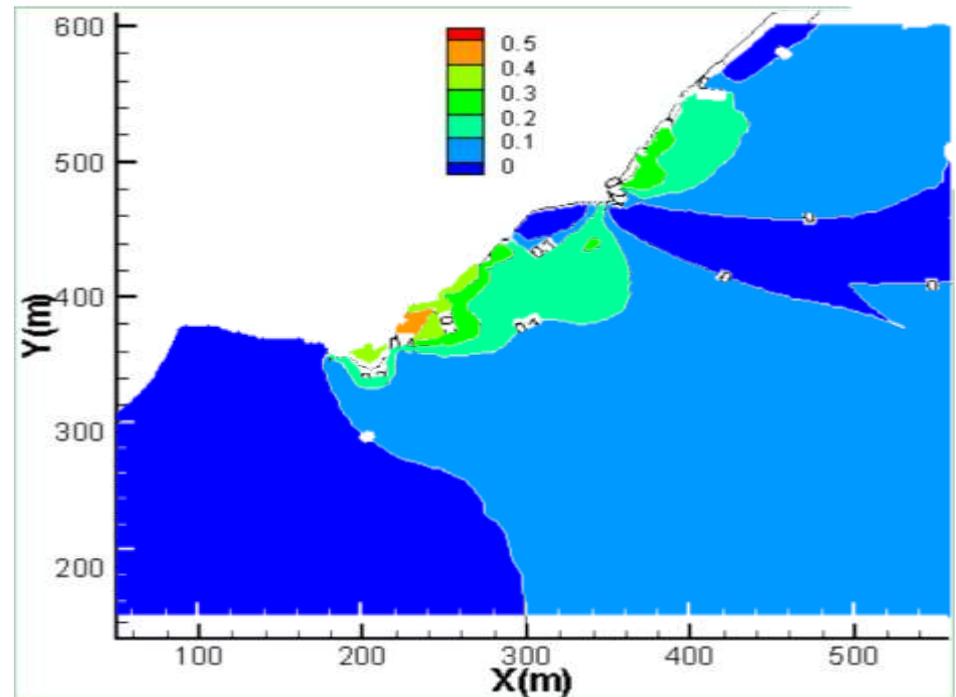
(1) Division of Excavation Damage Zone

Method of dividing Excavation Damage Zone

- In-situ stress measurement
- Acoustic wave test
- Numerical simulation



Distribution of horizontal stress

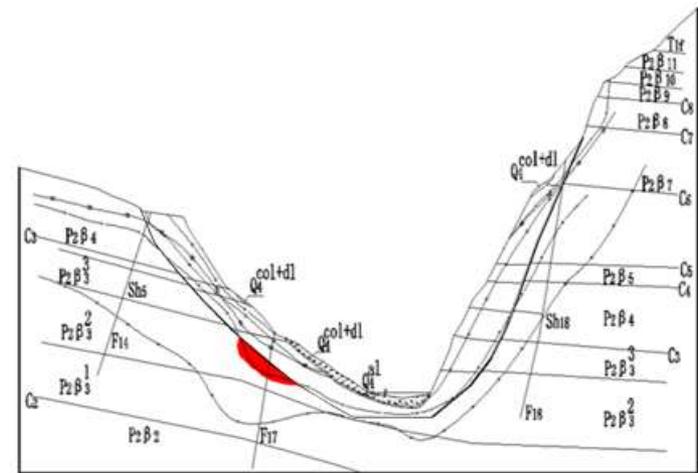
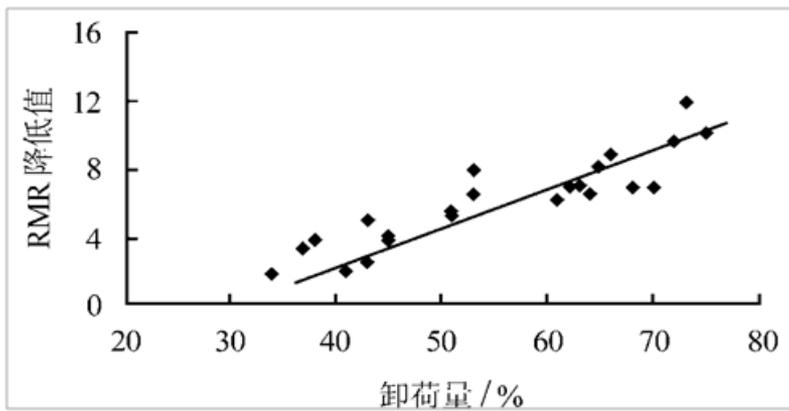


Distribution of point safety factor

3 Research Contents

(2) Quality Evaluation of Unloading Rock Masses

Excavation unloading effect of rock masses is introduced into RMR.



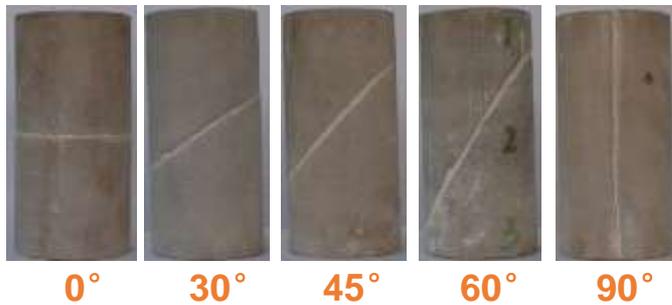
modified RMR

Quantity of unloading	<30	30~50	50~80	>80
Value of RMR	-4	-8	-14	-16

3 Research Contents

(3) Anisotropy of unloading rock masses

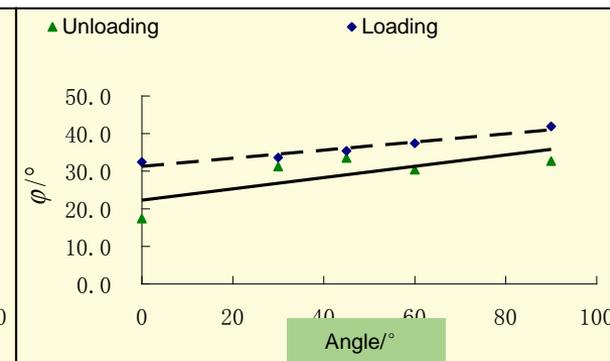
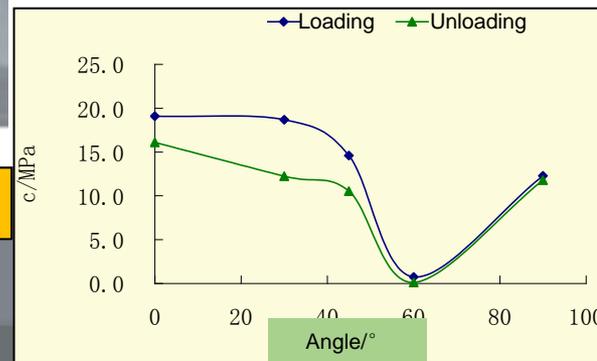
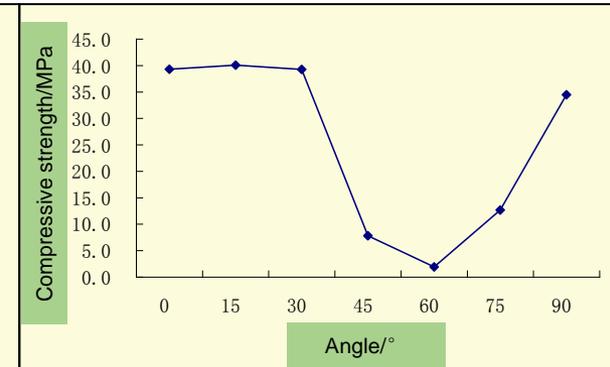
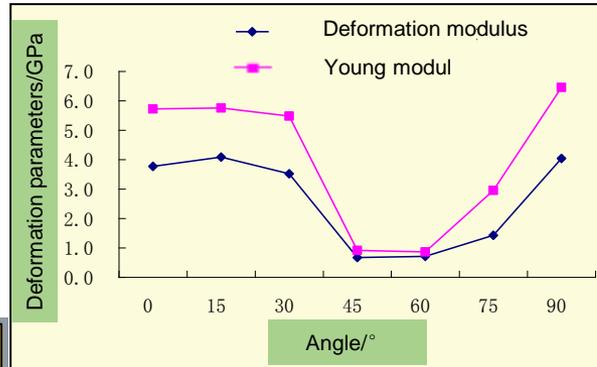
Anisotropic mechanical characteristics of jointed rock masses is revealed by experimental study.



Shear failure



sliding failure



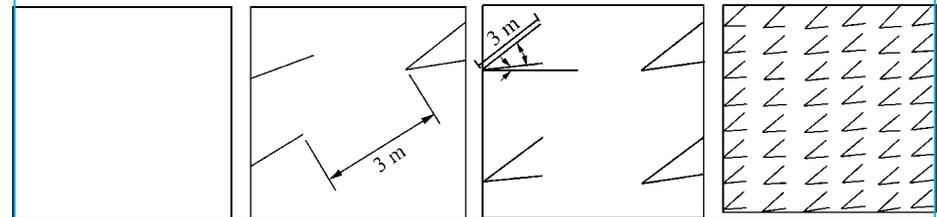
3 Research Contents

(4) Size Effect

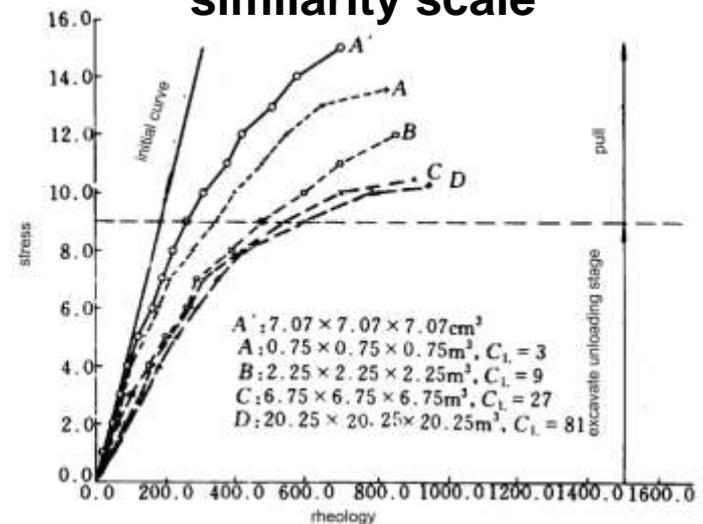
Four sets of discontinuities in the
Three Gorges Ship Lock



Model of jointed rock masses

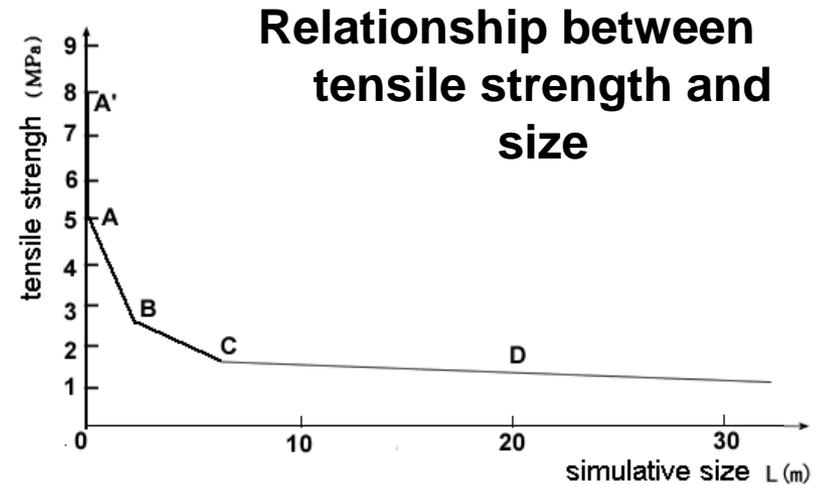
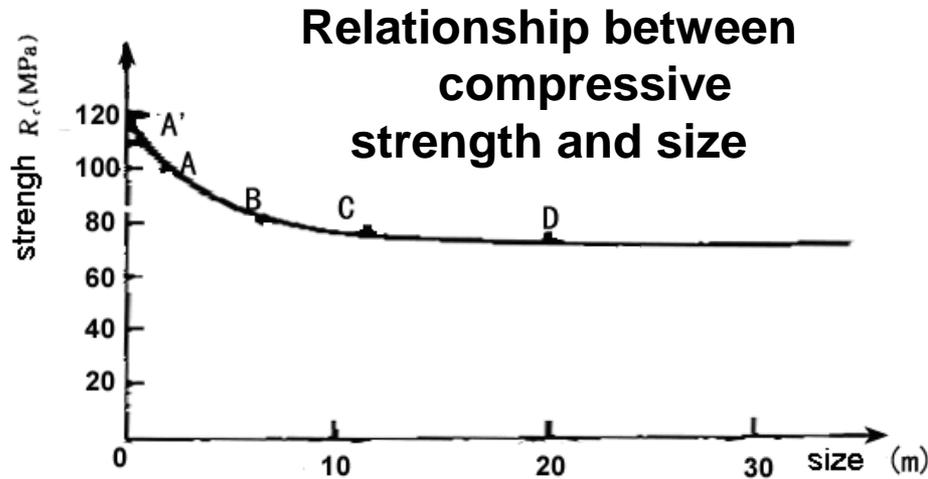


Unloading curves of different
geometric
similarity scale



3 Research Contents

(4) Size Effect



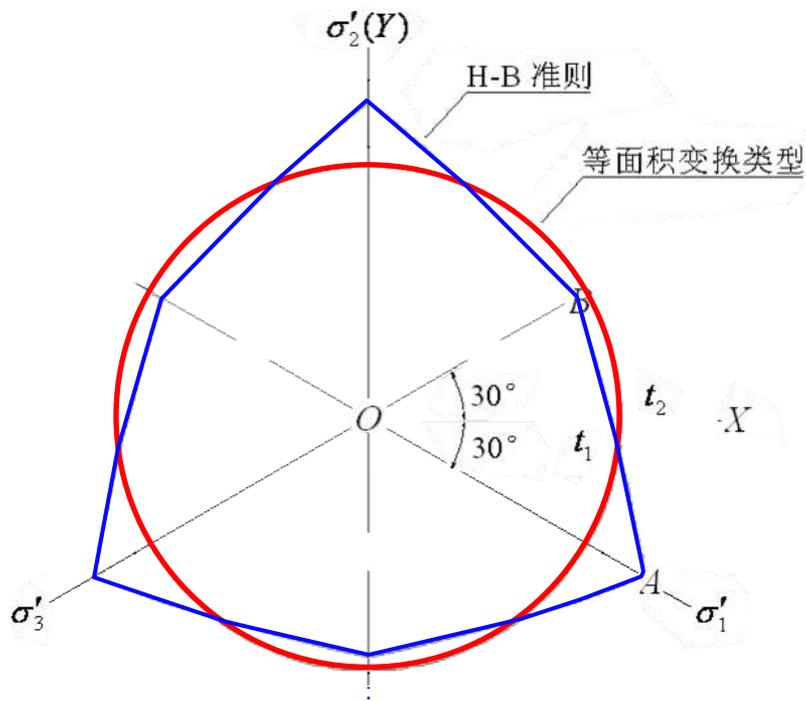
Deformation modulus varies with the size

Rock masses size(m)	0.75×0.75	2.25×2.25	6.75×6.75	20.25×20.25
Compressive deformation modulus (GPa)	50	45	38	35
Tensile deformation modulus (GPa)	6	4	2.0	1.5
Initial unloading modulus (GPa)	35	32	28	26

3 Research Contents

(5) Yield criterion for unloading rock masses

Drucker-Prager criterion is established by considering the shear failure characteristics of unloading rock masses.



Formulation of D-P criterion:

$$F = \alpha I_1 + J_2 + \beta \sqrt{J_2} - k = 0$$

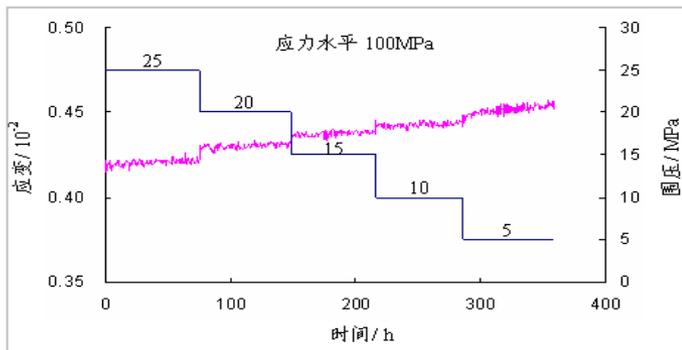
Material parameters:

$$\begin{cases} \alpha = -m\sigma_c / 12 \cos^2 \theta_\sigma \\ \beta = m\sigma_c (\sqrt{3} \sin \theta_\sigma + 3 \cos \theta_\sigma) / 12 \cos^2 \theta_\sigma \\ k = s\sigma_c^2 / 4 \cos^2 \theta_\sigma \end{cases}$$

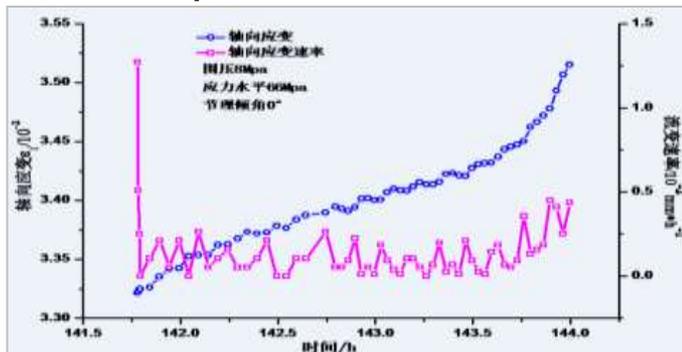
3 Research Contents

(6) Creep behavior

The nonlinear constitutive model of unloading creep for jointed rock masses is established.



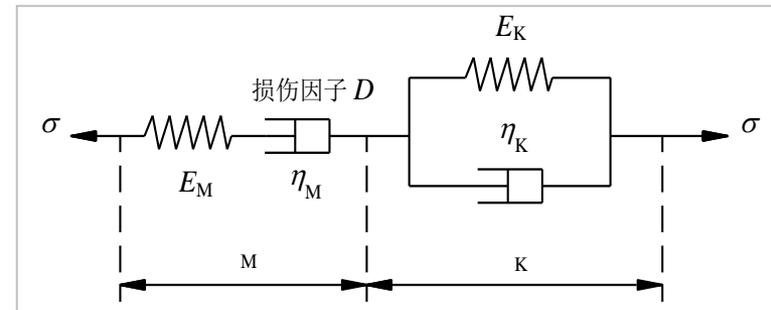
Creep behavior of intact rock



Creep behavior of jointed rock masses

Damage factor

$$D = 1 - (a\Delta\sigma)^{-b(t-t^*)}$$



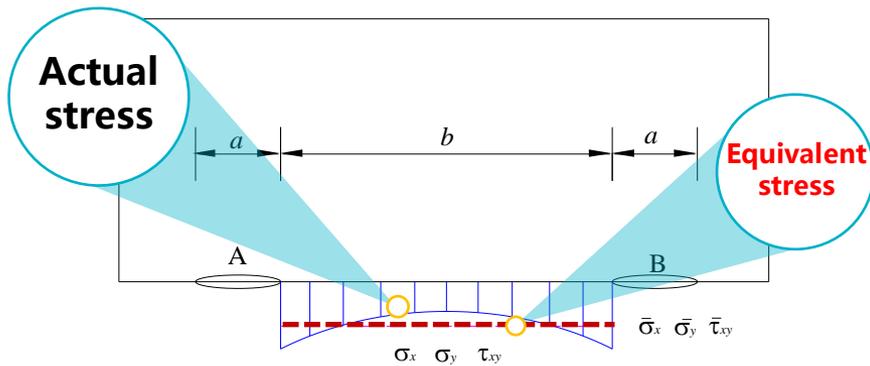
Nonlinear constitutive model

$$\begin{cases} \varepsilon = \frac{\sigma}{E_M} + \left(\frac{\sigma}{\eta_M}\right)t + \frac{\sigma}{E_K} \left(1 - e^{-\frac{E_K t}{\eta_K}}\right) & (t < t^*) \\ \varepsilon = \frac{\sigma}{E_M} + \left(\frac{\sigma}{\eta_M}\right) \left((a\Delta\sigma)^{b(t-t^*)}\right)t + \frac{\sigma}{E_K} \left(1 - e^{-\frac{E_K t}{\eta_K}}\right) & (t \geq t^*) \end{cases}$$

3 Research Contents

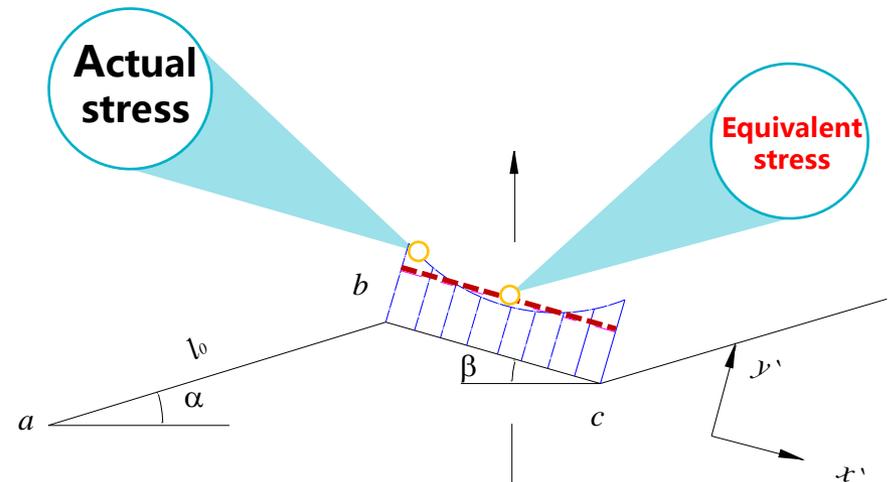
(7) Fracture behavior

An equivalent analytical model of compression shear and tension shear for unloading rock masses is proposed.



Compression-shear fracture

$$\left\{ \begin{array}{l} m = -\frac{\sqrt{\pi a(1/\varphi - 1)}\sigma_c}{\sqrt{2}K_{Ic}}s \\ 16K_{IIc}^2 + \sigma_c\sqrt{2\pi a(1/\varphi - 1)}K_{IIc}m = \frac{\pi a}{2}(1/\varphi - 1)\sigma_c s \end{array} \right.$$



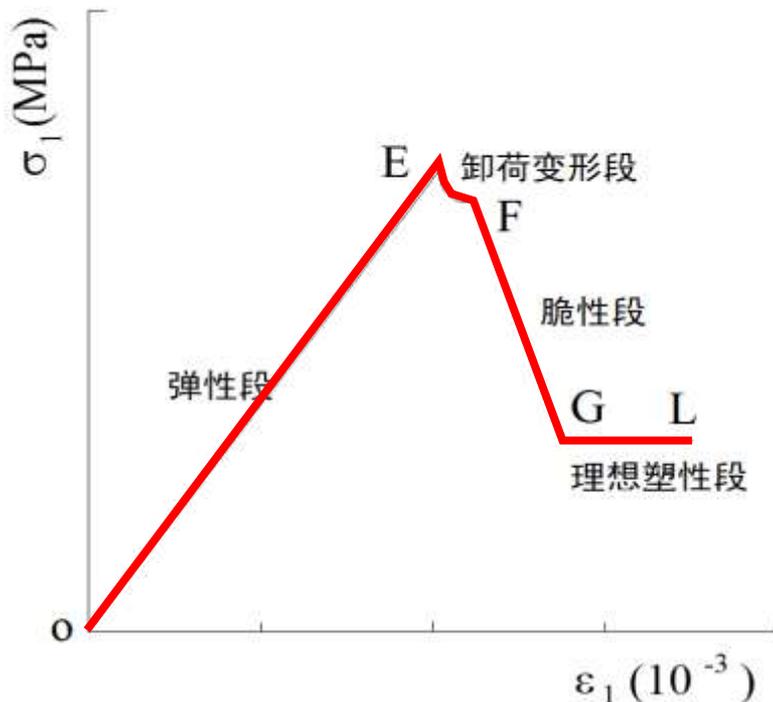
Tension-shear fracture

$$\left\{ \begin{array}{l} m = 16K_{IIc}^2 / \sqrt{2\pi}K_{Ic}(1 + K_{IIc} / K_{Ic}) \\ s = 32K_{IIc}^2 / \pi\sigma_c^2(1 + K_{IIc} / K_{Ic}) \end{array} \right.$$

3 Research Contents

(8) Constitutive model of unloading rock masses

An incremental constitutive model of unloading rock masses and a hyperbolic nonlinear elastic constitutive model of unloading rock masses are established.



Plastic deformation

$$\{d\sigma\} = \left(\begin{array}{c} [D]_e - \frac{\left\{ \frac{\partial F_{b-s}}{\partial \varepsilon} \right\}^T \left\{ \frac{\partial F_{b-s}}{\partial \varepsilon} \right\}}{A + \left\{ \frac{\partial F_{b-s}}{\partial \varepsilon} \right\}^T [C]_e \left\{ \frac{\partial F_{b-s}}{\partial \varepsilon} \right\}} \end{array} \right) \{d\varepsilon\}$$

Yield function

$$F_{b-s} = \frac{E - E^b}{E^s - E^b} f_b + \frac{E^s - E}{E^s - E^b} f_s = 0$$

Elastic-brittle-plastic constitutive model

3 Research Contents

(9) Determination of mechanical parameters for jointed rock masses

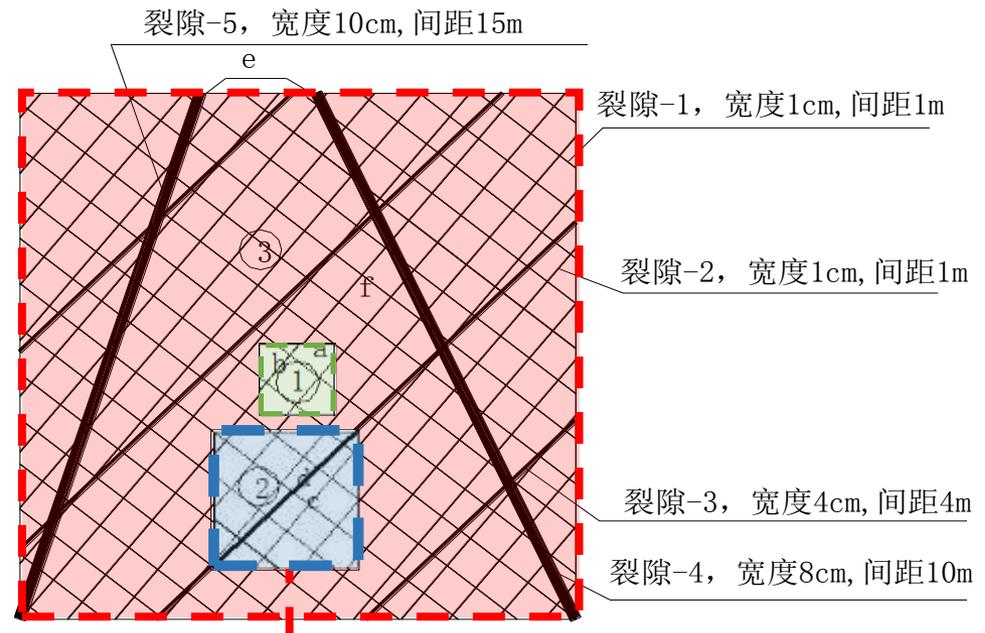
A method, which suggests starting from the small-size fracture to the large-size fracture to study the size effect of mechanical parameters, has been proposed to obtain mechanical parameters of jointed rock masses.



Jointed rock masses



Analytical model



3 Research Contents

(10) Inversion of mechanical parameters of unloading rock masses

Based on the artificial neural network, the excavation unloading effect has been considered in the inversion of rock mechanics parameters.

Deformation mechanism of unloading rock masses

Analytical model

Geological factor

Monitoring data

Inverse analysis

Predicting the deformation

In situ stress

Excavation

Support

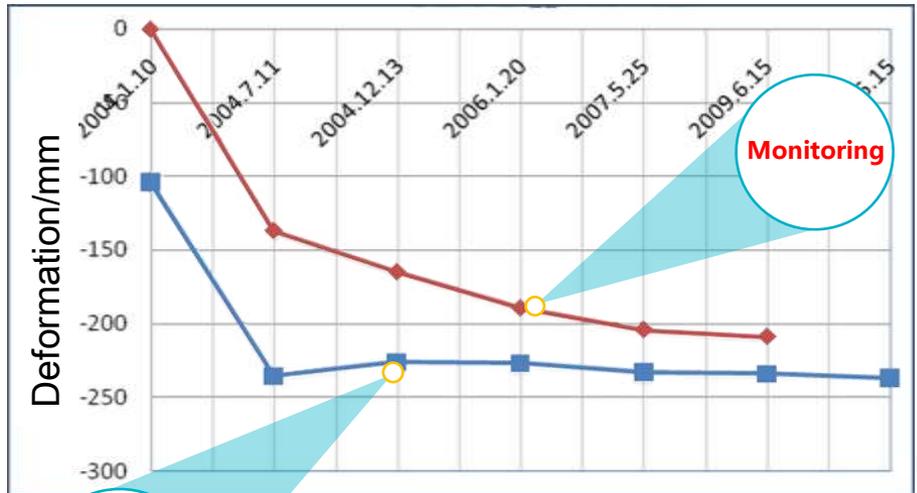
Impoundment

Rainfall

Earthquake

Creep

Comparison of calculation and monitoring in slope

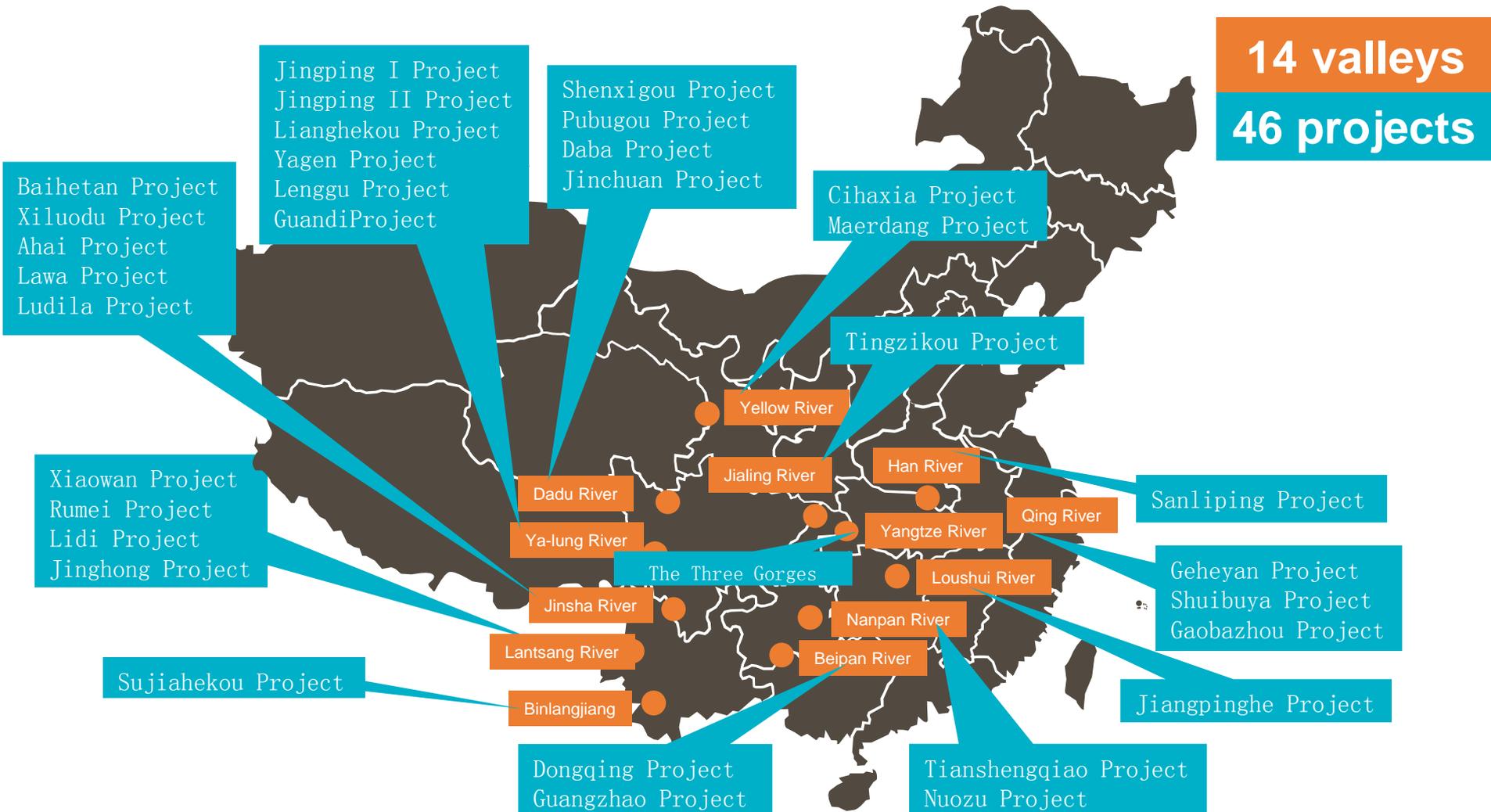


Calculation

Monitoring

4. ENGINEERING APPLICATION

4.1 Applied valley



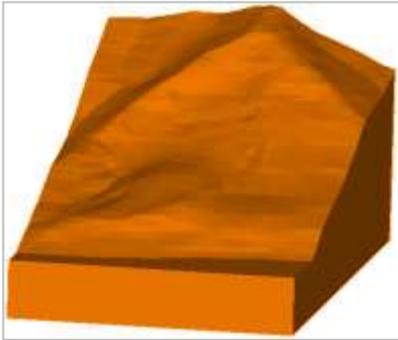
4. ENGINEERING APPLICATION

4.2 Applied Engineering

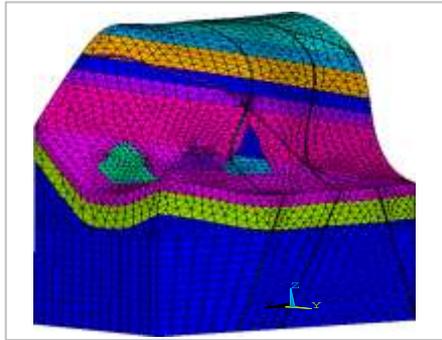


4. ENGINEERING APPLICATION

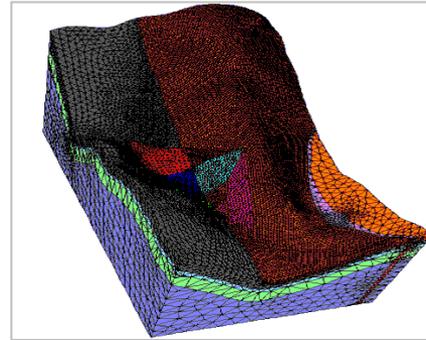
4.2 Applied Engineering



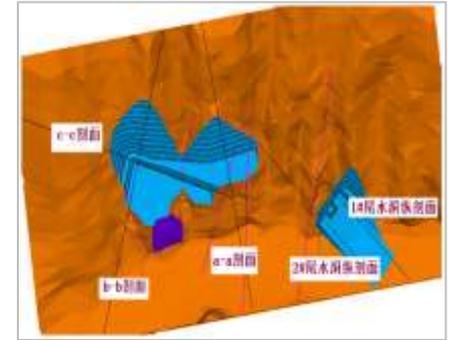
Landslide-Geheyuan



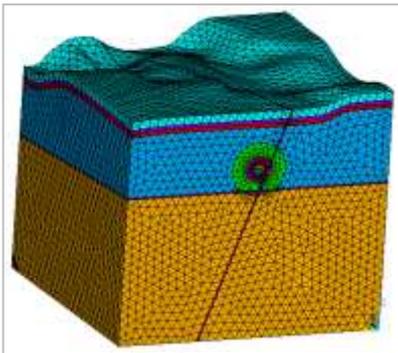
Slope-Jiangpinghe



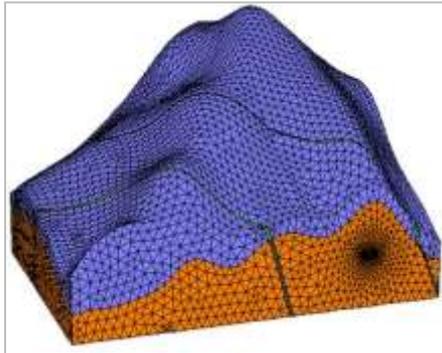
High slope-Rumei



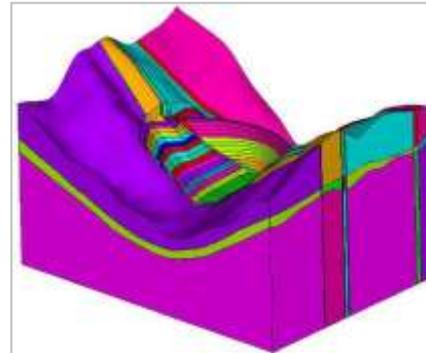
High slope-Jinchuan



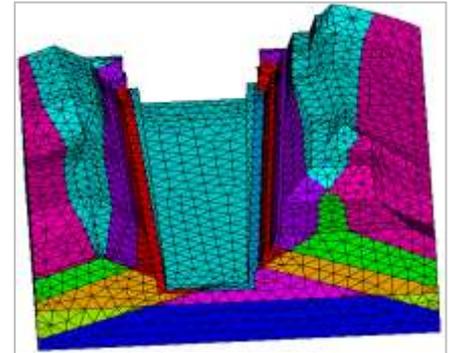
Tunnel-Dashankou



Tunnel-Danba



Slope-Xiaowan



Slope-Dongqing

5. RESEARCH PLATFORM

5.1 Introduction of CTGU

China Three Gorges University



China Three Gorges University



Three Gorges Dam



Gezhouba Dam



5. RESEARCH PLATFORM

5.2 Research team

Team members



5. RESEARCH PLATFORM

5.3 Research platform

- Key Laboratory of Geological Hazards on Three Gorges Reservoir Area (China Three Gorges University), Ministry of Education



The screenshot shows the website for the Key Laboratory of Geological Hazards on Three Gorges Reservoir Area (China Three Gorges University), Ministry of Education. The URL is <http://geoh.ctgu.edu.cn/>. The page features a navigation menu with items like '网站首页', '实验室概况', '研究队伍', '人才培养', '研究成果', '学术交流', '开放基金', '资源共享', '实验室新闻', '运行管理', and '联系我们'. Below the navigation are three main content areas with images and text. At the bottom, there are two columns of news and announcements.

通知公告 Announcement	更多 >	实验室新闻 News	更多 >
• 公布一教典球重点实验室五年工作总结报告	12-04	• 高松教授担任十二五科技支撑计划课题在武汉召开首次检查会	10-28
• 第五届全国水工抗震防灾学术交流会 (四)	11-06	• 第十二届国际非连续体分析会议在武汉成功召开	10-28
• 第五届全国水工抗震防灾学术交流会 (三)	11-05	• 加拿大Uterak大学教授Dave Chen受邀做报告	10-20
• 第五届全国水工抗震防灾学术交流会 (二)	11-05	• 三峡库区群钻岩、开山岭地区地质灾害专业监测站2013年中期工作总结一	10-20
• 第五届全国水工抗震防灾学术交流会 (一)	11-05	• 我校获国家科技一等奖赴香港进行学术交流	10-20
• 第十三届全国青年岩石力学与工程学会大会 2号通知	11-05	• 重庆大学杰出中青年教授周学华应邀做报告并在该院进行了学术讲座	10-11
• 2013年度基金委二区项目申报通知	11-05	• 重庆大学岩土博士朱洪波进行学术交流	10-11
• 学术报告——极端干旱气候条件下典型工程地质问题研究	11-05	• 我校采用无人扶遥控技术助力三峡库区地质灾害防治合作取得显著成效	09-18
• 研究、探讨和地震监测预警工程力学方法和经验	09-25	• 实验室学术骨干参加2013年全国工程地质学术大会	09-19
• 论坛我国岩土力学与工程工程难题	09-25	• 实验室研究人员参加“三峡水库库区沉降监测与库区地质灾害防治工程研讨会一	09-19



Monitoring System

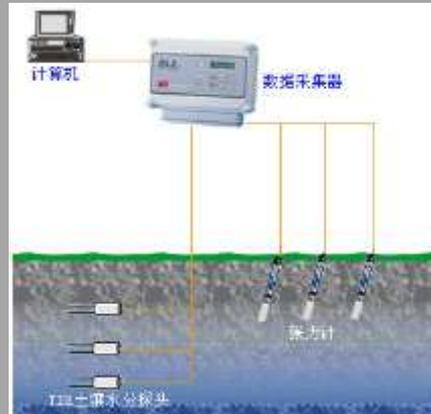
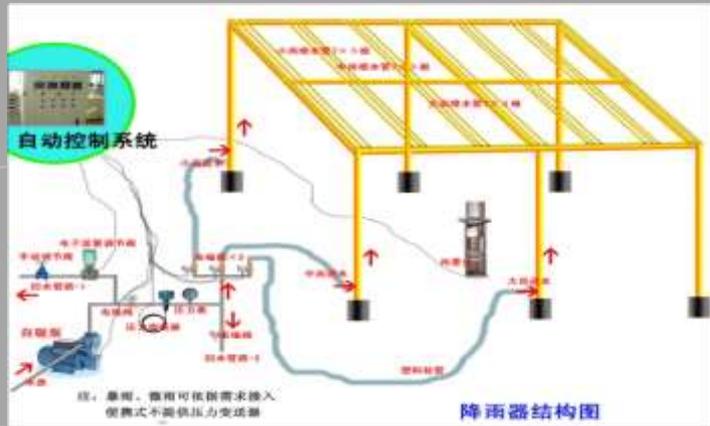
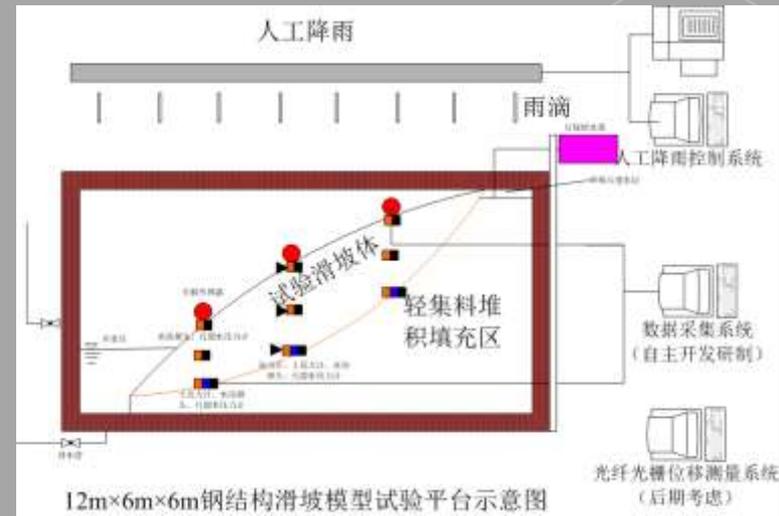
5. RESEARCH PLATFORM

5.3 Research platform

➤ Equipment (1)



Three dimensional landslide physical model test system (12m x 6m x 6m)



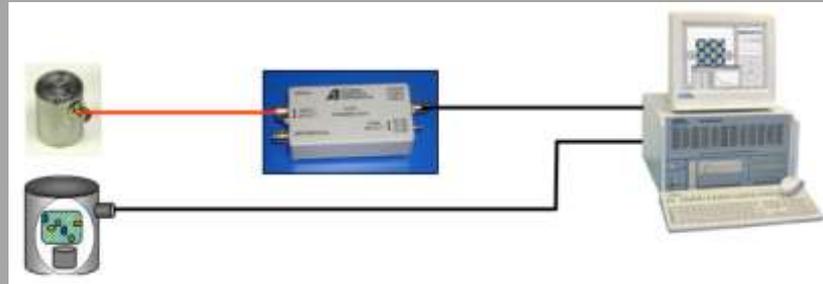
5. RESEARCH PLATFORM

5.3 Research platform

➤ Equipment (2)



ELE rock seepage system



PCI-2 acoustic emission detection system



ST500 three-dimensional non-contact surface profilometer



RMT-150C rock mechanics test system



Adaptive automatic triaxial testing machine



RLW-2000 triaxial creep test system

5. RESEARCH PLATFORM

5.3 Research platform

➤ Equipment (3) :



quadruple direct shear apparatus for unsaturated soil



JSM-7500F scanning electron microscope



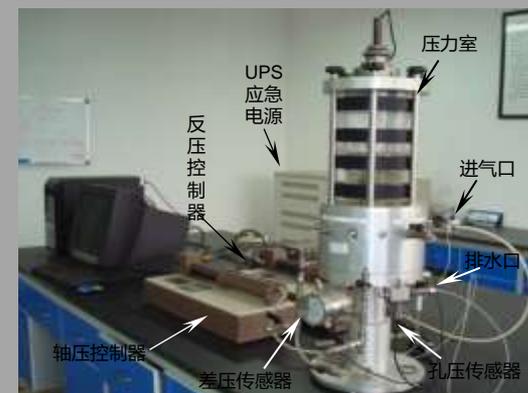
Computer controlled electro-hydraulic servo soil dynamic triaxial testing machine



DHJ-50 large single shear direct shear apparatus



The soil-water characteristic curve tester



HKUST-GDS unsaturated soil triaxial apparatus



Unloading Rock masses Mechanics
THANKS

2016.12